

TITLE OF THE INVENTION

METHOD OF MANUFACTURING GLASS SUBSTRATE FOR INFORMATION
RECORDING MEDIA, GLASS SUBSTRATE FOR INFORMATION
5 RECORDING MEDIA MANUFACTURED USING THE METHOD, AND
INFORMATION RECORDING MEDIUM USING THE GLASS SUBSTRATE

BACKGROUND OF THE INVENTION

10 Field of the Invention

The present invention relates to a method of
manufacturing a glass substrate for information recording
media, a glass substrate for information recording media
manufactured using the method, and an information
15 recording medium using the glass substrate.

Prior Art

Information recording media include magnetic disks,
optical magnetic disks and optical disks. A magnetic
20 disk, for example, generally has a donut shape with a
hole in the center thereof, and a magnetic film that acts
as a data recording medium is covered onto one or both
major surfaces of the disk. Data is recorded onto such a
magnetic disk by means of differences in strength of
25 magnetism.

A glass substrate for such a magnetic disk is
usually manufactured through a manufacturing process
described below.

FIG. 9 is a flow chart of a conventional
30 manufacturing process for a glass substrate for a
magnetic disk.

First, a starting material glass plate of thickness
1.0mm is prepared (step P1). Next, a donut-shaped glass
disk having an outside diameter of 84mm and an inside
35 diameter of 25mm is cut out from the starting material

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glass plate (step P2). The method of doing this is to irradiate with a laser beam along cutting lines to cause strain or insert cutting lines using a wheel cutter, and then cut along the cutting lines. The cutting lines run
 5 along the outer periphery and the inner periphery of the glass disk; the outer cutting line is set 0.5 to 1.0mm outside the outer periphery, and the inner cutting line 0.5 to 1.0mm inside the inner periphery.

The next step is to grind the cut-out surfaces at
 10 the outer and inner peripheries of the glass disk, thus adjusting the outside and inside diameters and also chamfering the cut-out surfaces (step P3). After the grinding, the average roughness Ra is, for example, 0.3 to 0.4 μ m, and the maximum roughness Rmax, for example, 3
 15 to 4 μ m. The grinding is carried out on one glass disk at a time, and is comprised of first stage grinding using a diamond grindstone of #324 roughness (coarse), and second stage grinding using a diamond grindstone of #500 roughness (fine). The chamfering is carried out at an
 20 angle of 45°, and 0.15mm is chamfered at a time.

Next, 30 or so of the glass disks are stacked on top of one another, and the outer peripheral edge surfaces of the glass disks are polished using an outer peripheral edge surface polishing machine (step P4), and then 100 or
 25 so of the glass disks are stacked on top of one another, and the inner peripheral edge surfaces of the glass disks are polished using an inner peripheral edge surface polishing machine (step P5). Each of these two polishing steps is carried out by pushing a rotating brush against
 30 the surfaces to be polished of the rotating stacked glass disks while spraying a cerium oxide slurry on the surfaces. After the polishing, the average roughness Ra is, for example, 0.05 to 0.4 μ m, and the maximum roughness Rmax, for example, 0.3 to 2.5 μ m.

35 The major surfaces of the glass disks are then

polished by sandwiching the glass disks at the major surfaces between two pads impregnated with a cerium oxide slurry and rotating (step P6). Next, abrasive grains and the like attached to the glass disks are washed off using warm water, alkaline washing water or pure water (step P7), and then the glass disks are strengthened using chemical strengthening treatment (step P8). Finally, salt from the chemical strengthening treatment, foreign matter and the like attached to the glass disks are once again washed off using warm water, alkaline washing water or pure water (step P9).

In general, the inside and outside peripheral edge surfaces of a magnetic disk are not used as data recording surfaces. Nevertheless, the inner and outer peripheral edge surfaces of the glass disk are ground and polished in steps P3 to P5 of the manufacturing process described above, because cracks and undulations inevitably remain on the cut-out surfaces at the inside and outside peripheries of the glass disk after the glass disk is cut out in step P2, and such cracks may lead to fracture of the glass disk, and moreover foreign matter such as abrasive grains that appear during the manufacturing process may collect in the recessed parts of such undulations, and this foreign matter may fly out when the glass disk is used as a magnetic disk and rotated at high speed, adversely affecting the recording surfaces.

The conventional method of manufacturing a glass substrate for information recording media described above, however, suffers from the following problems:

(1) The grinding/chamfering step P3 and the polishing steps P4 and P5 are time-consuming and costly, and moreover variation in surface roughness between glass disks and variation in surface roughness from place to place on a single glass disk occur.

5 (2) Setting of glass disks must be carried out separately for the inner peripheral edge surface polishing machine and the outer peripheral edge surface polishing machine, and hence many operators are required, and the cost is high.

10 (3) To improve the processing efficiency, polishing is carried out simultaneously on 100 or so glass disks stacked on top of one another using the inner peripheral edge surface polishing machine, and 30 or so glass disks stacked on top of one another using the outer peripheral edge surface polishing machine, and hence the major surfaces of the glass disks rub against one another and may become scratched.

15 (4) Even though the inner and outer peripheral edge surfaces of each glass disk are smoothed by chamfering and polishing in steps P3 to P5, fine cracks of depth, for example, 1 to 60 μ m may remain, resulting in the strength of the glass dropping. Moreover, if there are cracks or the like on the inner and outer peripheral edge surfaces of the glass disk, then the strength will not increase sufficiently even if chemical strengthening treatment is carried out.

20 (5) Large-grained glass powder generated during the grinding in step P3 may adhere to the major surfaces of the glass disk, resulting in scratches.

30 (6) In step P5 in particular, uneven polishing may occur due to the rotating brush not contacting the stacked glass disks uniformly, resulting in the problem of the extent of polishing varying between the glass disks.

SUMMARY OF THE INVENTION

35 It is an object of the present invention to provide a method of manufacturing a glass substrate for

information recording media that allows the inner and outer peripheral edge surfaces of the glass substrate for information recording media to be smoothed easily and inexpensively, a glass substrate for information

5 recording media manufactured using this method, and an information recording medium using this glass substrate.

To attain the above object, the present invention provides a method of manufacturing a glass substrate for information recording media, comprising the steps of
10 preparing a donut-shaped glass disk for information recording media having an outer peripheral edge surface and an inner peripheral edge surface, and smoothing at least one of the outer peripheral edge surface and the inner peripheral edge surface of the glass disk by melt-
15 heating to a temperature at or above the softening point of the glass by irradiating with at least one laser beam. As a result, at least one of the outer peripheral edge surface and the inner peripheral edge surface of the glass disk becomes smooth and rounded, and hence a
20 polishing step used in a conventional method can be omitted, and moreover chamfering in a grinding step can also be omitted.

Preferably, both the outer peripheral edge surface and the inner peripheral edge surface are melt-heated in
25 the smoothing step. As a result, the working efficiency can be improved.

Also preferably, the at least one laser beam is a divergent beam. As a result, the at least one laser beam can be reliably prevented from being irradiated onto and
30 thus melting the at least one major surface of the glass disk.

Also preferably, the ratio of the energy density of the laser beam on the outer peripheral edge surface to the energy density of the laser beam on the inner
35 peripheral edge surface is in a range of 2 to 5. As a

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result, the energy density per unit area can be made approximately the same for the inner peripheral edge surface and the outer peripheral edge surface.

Also preferably, the mother glass of the glass disk
5 is a silicate glass containing one compound selected from the group consisting of Li_2O and Na_2O as an alkaline oxide component, and chemical strengthening treatment is carried out wherein an alkaline component in a surface layer of the glass disk which has been subjected to the
10 smoothing is replaced with an alkaline component having an ionic radius larger than the ionic radius of the alkaline oxide component. As a result, the strength of the glass disk can be increased.

To attain the above object, the present invention
15 also provides a glass substrate for information recording media manufactured using the method according to the present invention as described above. As a result, a glass substrate wherein at least one of the inner peripheral edge surface and the outer peripheral edge
20 surface is smooth can be obtained.

To attain the above object, the present invention
also provides an information recording medium comprising the glass substrate for information recording media according to the present invention as described above
25 with an information recording film formed on at least one major surface thereof. As a result, an information recording medium wherein foreign matter does not attach to the major surface(s) thereof can be obtained.

Also, according to the present invention, an
30 information recording medium can be obtained by forming an information recording film such as a magnetic recording film, an optical magnetic recording film or an optical recording film on one or both major surfaces of the glass substrate for information recording media
35 according to the present invention as described above.

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The above and other objects, features and advantages of the invention will become more apparent from the following detailed description taken in conjunction with
5 the accompanying drawings.

FIG. 1 is a flow chart of a manufacturing process for a glass substrate for information recording media according to an embodiment of the present invention;

FIG. 2 is a partially sectional view of an example of a laser beam irradiation apparatus used in step P14 shown in FIG. 1;

FIG. 4 is a view useful in explaining a mirror in
20 the laser beam irradiation apparatus shown in FIG. 2;

FIGS. 6A and 6B are views useful in explaining the
25 roughness of a peripheral edge surface of a glass disk;
specifically:

FIG. 6B shows the peripheral edge surface after the
30 laser beam irradiation of step P14;

35 FIG. 8 is a graph showing the frequency distribution

FIG. 9 is a flow chart of a conventional manufacturing process for a glass substrate for a magnetic disk.

Embodiments of the method of manufacturing a glass
10 substrate for information recording media according to
the present invention will now be described with
reference to the drawings.

First, a starting material glass plate of thickness 1.0mm is prepared (step P11). The mother glass of this starting material glass plate is preferably a silicate glass that is rigid and resistant to chemicals such as alkalis, a crystallized glass made by crystallizing a silicate glass through heat treatment, or the like.

Examples of the silicate glass include soda lime
30 silicate glass which is used as window glass in building,
aluminosilicate glass, borosilicate glass, and glass that
can be easily chemically strengthened. The glass that
can be easily chemically strengthened is a glass which is
chemically strengthened by bringing the glass into
35 contact with molten potassium nitrate to replace lithium

ions and/or sodium ions in the glass with potassium ions, which have a larger ionic radius than lithium ions and sodium ions, or by bringing the glass into contact with molten sodium nitrate to replace lithium ions in the

5 glass with sodium ions, which have a larger ionic radius than lithium ions, thus producing compressive stress in a surface layer (depth about 50 to 200 μ m) of the glass. An example of this type of glass contains as principal components 60 to 65mass% of SiO₂, 10 to 20mass% of Al₂O₃,

10 0 to 5mass% of MgO, 0 to 5mass% of CaO, 2 to 10mass% of Li₂O, and 5 to 15mass% of Na₂O. Moreover, a crystallized glass has principal components selected from SiO₂, Al₂O₃, Li₂O, MgO, P₂O₃, ZrO, CeO₂, TiO₂, Na₂O and K₂O.

There are no particular limitations on the

15 composition of the crystallized glass, but a crystallized glass containing, for example, 70 to 80mass% of SiO₂, 2 to 8mass% of Al₂O₃, 1 to 7mass% of K₂O, 5 to 15mass% of Li₂O and 1 to 5mass% of P₂O₅ is preferable, as such a glass does not suffer heat fracture when irradiated with

20 a laser beam, and hence edge surfaces thereof can be smoothed using step P14 described below.

The starting material glass plate is formed using a float glass manufacturing method, a down-draw manufacturing method, or the like.

25 A donut-shaped glass disk having an outside diameter of 84mm and an inside diameter of 25mm is cut out from the starting material glass plate (step P12). The method of doing this is to irradiate with a laser beam along the cutting lines to cause strain or insert the cutting lines

30 using a wheel cutter, and then cut along the cutting lines. The cutting lines run along the outer periphery and the inner periphery of the glass disk; the outer cutting line is set 0.5 to 1.0mm outside the outer periphery, and the inner cutting line 0.5 to 1.0mm inside

35 the inner periphery.

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The next step is to grind the cut-out surfaces at the outer and inner peripheries of the glass disk, thus adjusting the outside and inside diameters (step P13). After the grinding, the average roughness R_a is, for example, 0.3 to 0.4 μm , and the maximum roughness R_{max} , for example, 3 to 4 μm . The grinding is carried out on one glass disk at a time, and is comprised of first stage grinding using a diamond grindstone of #324 roughness (coarse), and second stage grinding using a diamond grindstone of #500 roughness (fine).

Next, edge surface smoothing is carried out by irradiating a laser beam onto each of the inner peripheral edge surface and the outer peripheral edge surface of the glass disk using a laser beam irradiation apparatus, described below, thus heating the inner peripheral edge surface and the outer peripheral edge surface of the glass disk to a temperature at or above the softening point of the glass, for example 750°C or more, preferably about 1000°C, and hence melting or making fluid projecting parts of the inner and outer peripheral edge surfaces of the glass disk and thus smoothing the inner and outer peripheral edge surfaces (step P14). As a result, compressed layers can be formed on the inner and outer peripheral edge surfaces without scratches or fine cracks appearing. The mechanical strength of the glass disk can thus be increased.

The major surfaces (information recording surfaces) of the glass disk that will be covered with information recording films are then ground using diamond grindstones and precision polished using a cerium oxide suspension, thus making the thickness of the glass disk a predetermined value and smoothing the surfaces (step P15). Washing is then carried out to remove abrasive grains used in the polishing and the like (step P16).

Next, the glass disk is further strengthened using

chemical strengthening treatment, so that the strength will be sufficient when the glass disk is rotated at high speed during use as an information recording medium (step P17). In the chemical strengthening treatment, to
5 strengthen the glass disk, alkaline metal ions in a surface layer of the glass disk are replaced with alkaline metal ions having a larger ionic radius, thus forming a compressed layer. Specifically, the chemical strengthening treatment is carried out by immersing the
10 glass disk in a molten salt at 400 to 450°C for 2 to 5 hours. If the molten salt is potassium nitrate (KNO_3), then lithium ions and sodium ions in the surface layer of the glass disk are replaced with potassium ions, whereas if the molten salt is sodium nitrate (NaNO_3), then
15 lithium ions in the surface layer of the glass disk are replaced with sodium ions.

Finally, the glass disk that has been subjected to the chemical strengthening treatment is washed using warm water, alkaline washing water or pure water, thus
20 removing salt from the chemical strengthening treatment, foreign matter and the like attached to the glass disk (step P18).

FIG. 2 is a partially sectional view of an example of the laser beam irradiation apparatus used in step P14
25 shown in FIG. 1.

In FIG. 2, a disk-shaped horizontal worktable 11 is connected to a vertical shaft 12, and is rotated about the vertical shaft 12 by a motor, not shown. A glass disk 14 for making a magnetic disk is placed on an upper
30 surface of the worktable 11 via two annular seats 13, and thus rotates with the worktable 11. The glass disk 14 has been cut out from a starting material glass plate and inner and outer peripheral edge surfaces 15 and 16 thereof have been ground in steps P11 to P13 described
35 above.

An annular groove 17 is formed in the upper surface of the worktable 11 in concentricity with the worktable 11. A thermal insulating material 18 is fitted in the groove 17 and disposed along side walls and a bottom wall thereof, and an electrical heater 19 is inserted into the groove 17 for preheating the glass disk 14.

The laser beam irradiation apparatus has a single laser oscillator 20. The laser oscillator 20 emits a laser beam in a horizontal direction, and the emitted laser beam is made into a parallel laser beam 22 by a collimator 21. The laser beam 22 is then alternately switched between a horizontal laser beam 24 and a vertical laser beam 25 by means of a galvano-scan mirror 23. The laser beam 24 is irradiated via two stationary mirrors 26 and 27 onto the inner peripheral edge surface 15 of the glass disk 14, and the laser beam 25 is irradiated via one stationary mirror 28 onto the outer peripheral edge surface 16 of the glass disk 14.

In the laser beam irradiation apparatus of FIG. 2, the speed of rotation of the worktable 11 is set such that the circumferential speed at the inner peripheral edge surface 15 of the glass disk 14 is 0.02 to 5.0 m/minute.

The laser oscillator 20 may be, for example, a YAG laser or a carbon dioxide laser, but a carbon dioxide laser is particularly preferable from the standpoint of the absorption coefficient.

The dominant wavelength of the laser beam emitted from the laser oscillator 20 is preferably 250 to 20,000nm, more preferably 900 to 12,000nm.

If the energy densities of the laser beams 24 and 25 are too low, then the temperature of the glass will not be raised sufficiently, but it is pointless to make these energy densities too high since this will not result in any further increase in the melting rate of the glass

surfaces. The energy densities of the laser beams 24 and 25 are thus preferably in a range of 1 to 20W/mm², more preferably 1 to 10W/mm².

The powers of the laser beams 24 and 25 are thus preferably in a range of 0.7 to 100W. Moreover, the ratio of the energy density of the laser beam 25 to the energy density of the laser beam 24 is preferably more than 1, and more preferably equal to the ratio of the outside diameter of the glass disk to the inside diameter thereof. As a result, the laser beam irradiation dose per unit length of the inner/outer peripheral edge surface of the glass disk will be the same for the inner and outer peripheral edge surfaces. Specifically, Table 1 shows the ratio of the outside diameter to the inside diameter for various nominal magnetic disk sizes, and it can be seen from Table 1 that this ratio is in a range of 2.8 to 4.0; the above energy density ratio is thus preferably in a range of 2 to 5.

Table 1

| Nominal size of glass substrate for recording media | 1" | 1.8" | 1.8" | 2.5" | 3" | 3.5" |
|---|-----|------|------|------|-----|------|
| Outside diameter (mm ϕ) | 27 | 48 | 48 | 65 | 84 | 95 |
| Inside diameter (mm ϕ) | 7 | 12 | 17 | 20 | 25 | 25 |
| Ratio (Outside diameter / Inside diameter) | 3.9 | 4.0 | 2.8 | 3.3 | 3.4 | 3.8 |

An energy density ratio as described above can be realized by adjusting the time for which the galvano-scan mirror 23 is stopped in each position.

In the laser beam irradiation apparatus constructed as above, the laser beam 22 may be alternately switched between the laser beam 24 irradiated onto the inner

peripheral edge surface 15 of the glass disk 14 and the laser beam 25 irradiated onto the outer peripheral edge surface 16 of the glass disk 14 using a semicircular plate-shaped mirror (chopper) 31 rotated by a motor 30 as shown in FIG. 3 instead of the galvano-scan mirror 23. Another alternative may be to split the laser beam 22 into two laser beams 24 and 25 using a stationary half mirror, not shown in the drawings, whereby the laser beam 24 can be irradiated onto the inner peripheral edge surface 15 of the glass disk 14 and the laser beam 25 onto the outer peripheral edge surface 16 of the glass disk 14 simultaneously. In this case, the ratio of the power of the laser beam 25 to the power of the laser beam 24 can be changed by changing the reflectance of the half mirror.

Moreover, the mirrors 27 and 28 are preferably convex as shown in FIG. 4. As a result, the laser beams 24 and 25 irradiated onto the inner and outer peripheral edge surfaces 15 and 16 respectively of the glass disk 14 can each be made into a divergent beam 29, and hence the laser beams 24 and 25 can be reliably prevented from being irradiated onto and thus melting the major surfaces of the glass disk 14. The angle of opening of the divergent beam is preferably 1 to 3 degrees. It goes without saying that the laser beams 24 and 25 may also be made divergent by not completely parallelizing the laser beam using the collimator 21, instead of using convex mirrors 27 and 28.

FIG. 5 is a partially sectional view of a modified example of the laser beam irradiation apparatus used in step P14 shown in FIG. 1.

In FIG. 5, a donut-shaped horizontal worktable 41 is connected to a vertical shaft 43 via a cap-shaped connecting portion 42, and is rotated about the vertical shaft 43 by a motor, not shown. A glass disk 46 for

making a magnetic disk is placed on an upper surface of the worktable 41 via two annular seats 44, and thus rotates with the worktable 41.

5 The glass disk 46 has been manufactured in the same way as the glass disk 14 shown in FIG. 2, and has an inner peripheral edge surface 47 and an outer peripheral edge surface 48. Moreover, a heater for preheating the glass disk 46 is provided along with a thermal insulating material in a groove in the upper surface of the
10 worktable 41 as in the case of the worktable 11 shown in FIG. 2, but these items have been omitted from FIG. 5.

The laser beam irradiation apparatus has a laser oscillator 50 for the outer peripheral edge surface 48 of the glass disk 46 and a laser oscillator 51 for the inner
15 peripheral edge surface 47 of the glass disk 46. The laser beam emitted from the laser oscillator 50 is made into a parallel laser beam 53 by a collimator 52, and the laser beam 53 is then irradiated onto the outer peripheral edge surface 48 of the glass disk 46 via a
20 mirror 54. The laser beam emitted from the laser oscillator 51, on the other hand, is made into a parallel laser beam 56 by a collimator 55, and then the laser beam 56 is alternately switched between traveling above and traveling below the glass disk 46 by means of a galvano-
25 scan mirror 57 disposed at the same height as the glass disk 46. The resulting laser beams 60 and 61 are irradiated alternately onto the inner peripheral edge surface 47 of the glass disk 46 via mirrors 58 and 59 respectively. This results in laser beam irradiation
30 being uniformly carried out over the inner peripheral edge surface 47. The connecting portion 42 has suitable openings 62 provided therein such that the laser beam 61 is not obstructed. The positions of the openings 62 can be calculated and set in accordance with the relationship
35 between the speed of operation of the galvano-scan mirror

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57 and the speed of rotation of the worktable 41.

In the laser beam irradiation apparatus constructed as above, a semicircular plate-shaped mirror rotated by a motor or a stationary half mirror may be used instead of the galvano-scan mirror 57, as with the laser beam irradiation apparatus of FIG. 2. Moreover, it goes without saying that the setting of the ratio of the energy density of the laser beam 61 to the energy density of the laser beam 60, the possibility of making the mirrors 54, 58 and 59 convex, and so on are as was described in the case of the laser beam irradiation apparatus of FIG. 2.

In the embodiments described above, the inner and outer peripheral edge surfaces of the glass disk 14 (or 46) were both irradiated with a laser beam, but only one of the inner and outer peripheral edge surfaces may be irradiated with a laser beam.

Moreover, in the embodiments described above, the size of the glass disk 14 (or 46) was an outside diameter of 84mm, an inside diameter of 25mm, and a thickness of 1.0mm. However, it goes without saying that the outside diameter, the inside diameter and the thickness may take any values.

According to the manufacturing process of FIG. 1, roughness in an amount corresponding to the diamond grindstones remains on the inner and outer peripheral edge surfaces 15 (or 47) and 16 (or 48) of the glass disk 14 (or 46) immediately before the laser beam irradiation of step P14 as shown in FIG. 6A, but the inner and outer peripheral edge surfaces 15 (or 47) and 16 (or 48) of the glass disk 14 (or 46) immediately after the laser beam irradiation of step P14 are smooth and edge portions adjoining the major surfaces are rounded as shown in FIG. 6B. That is, by carrying out the laser beam irradiation (step P14) on the inner and outer peripheral edge

surfaces to smooth these edge surfaces, polishing of the inner and outer peripheral edge surfaces (steps P4 and P5 in FIG. 9) which is conventionally carried out to smooth these edge surfaces can be omitted, and moreover
5 chamfering (step P3 in FIG. 9) which is conventionally carried out just before the smoothing of the edge surfaces can also be omitted.

According to the present invention, the smoothing (step P14) of the inner and outer peripheral edge
10 surfaces is carried out by melting or making fluid projecting parts of the inner and outer peripheral edge surfaces of the glass disk through laser beam irradiation. It is thought that melting and flowing of the glass in recessed parts of the inner and outer peripheral edge
15 surfaces also occurs at the same time. The projecting parts of the inner and outer peripheral edge surfaces thus flow into the recessed parts, and hence the surface is smoothed rapidly. Moreover, the smoothing is carried out in a dry state with only a laser beam coming into
20 contact with the glass disk and without abrasive grains or fine metal oxide particles such as cerium oxide particles being used, and hence the glass is not soiled and foreign matter does not become attached to the glass. Furthermore, by focusing the laser beam energy onto the
25 inner and outer peripheral edge surfaces of the glass disk, the smoothing can be carried out in a short time.

In contrast, in the case of the smoothing carried out conventionally on the inner and outer peripheral edge surfaces of a glass disk by chamfering and polishing
30 (steps P3 to P5 in FIG. 9), projecting parts are ground down progressively from the top, and hence the polishing must be carried out until the ground surface reaches the bottom of the recessed parts. To do this while insuring adequate industrial productivity, coarse abrasive grains
35 which give a high grinding rate may be used, but then

there is a limit to how smooth the surface can be made. To achieve a good balance between the grinding rate and the degree of smoothing, usually a plurality of stages of grinding are carried out, each with a different size of abrasive grains, but this results in problems such as the equipment cost being high due to a plurality of pieces of equipment being required and the processing taking a long time. A characteristic of the smoothing according to the present invention is that these drawbacks suffered by the conventional art are not present.

A description will now be given of examples of the present invention.

In these examples, the undermentioned experiments were carried out with regard to the samples shown in Table 2.

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Table 2

| | Type of glass | Glass disk edge surface smoothing steps | | | | Roughness of inner and outer peripheral edge surfaces | | | |
|---------------------|---------------|---|--|--|----------------------------------|---|-----------------------------------|-------------|---------------|
| | | Wet processing steps carried out | | | Dry processing steps carried out | Average roughness Ra (μ m) | Maximum roughness Rmax (μ m) | Δ Ra | Δ Rmax |
| | | First stage grinding using #324 roughness diamond abrasive grains | Second stage grinding using #500 roughness diamond abrasive grains | Precision polishing using suspension of cerium oxide fine powder | | | | | |
| Example | 1 | Yes | Yes | Yes | Yes | 0.03~0.06 | 0.2~0.5 | 0.03 | 0.3 |
| | 2 | Yes | Yes | — | Yes | 0.03~0.07 | 0.2~0.5 | 0.04 | 0.3 |
| | 3 | Yes | — | — | Yes | 0.06~0.10 | 0.4~0.7 | 0.04 | 0.3 |
| | 4 | Yes | Yes | — | Yes | 0.03~0.04 | 0.2~0.3 | 0.01 | 0.1 |
| Comparative example | 1 | Yes | Yes | — | — | 0.6~1.3 | 2.5~5.0 | 0.7 | 2.5 |
| | 2 | Yes | Yes | Yes | — | 0.05~0.4 | 0.3~2.5 | 0.35 | 2.2 |

Samples of a glass substrate for a magnetic disk of outside diameter 84mm, inside diameter 25mm and thickness 0.8mm were prepared through step 1 to step 8 in that order as described below.

A starting material glass plate was prepared by forming an aluminosilicate glass having 63.3mass% of SiO_2 , 16.3mass% of Al_2O_3 , 0.4mass% of K_2O , 1.9mass% of MgO , 3.8mass% of CaO , 3.7mass% of Li_2O , and 10.6mass% of Na_2O as principal components into a plate shape using a float glass manufacturing method.

500 glass disks were produced by inserting cutting lines into a surface of the starting material glass plate at a position slightly outside the above-mentioned outside diameter and a position slightly inside the above-mentioned inside diameter using a diamond cutter, and cutting out along the cutting lines by applying an external force.

Step 3A) First stage grinding of inner and outer peripheral edge surfaces

Each glass disk was fixed in a fixing jig, rotating grindstones having #324 roughness diamond abrasive grains attached thereto were pushed against the edge surfaces of the glass disk, and grinding was carried out until the inside diameter and the outside diameter became the predetermined values.

Step 3B) Second stage grinding of inner and outer peripheral edge surfaces

Each glass disk was fixed in a fixing jig, rotating grindstones having #500 roughness diamond abrasive grains attached thereto were pushed against the edge surfaces of

the glass disk, and the roughness of the edge surfaces was reduced. Afterwards, the glass disk was washed with water.

Step 3C) Precision polishing of inner and outer peripheral edge surfaces

100 of the glass disks for which the inner peripheral edge surface and the outer peripheral edge surface had been ground as above were stacked on top of one another and fixed, and, as shown in FIG. 7, precision polishing of the inner and outer peripheral edge surfaces was carried out by pushing cylindrical rotating brushes 4 and 5 made of a resin against the inner peripheral edge surfaces 2 and the outer peripheral edge surfaces 3 of the stacked glass disks 1 and feeding in a suspension containing cerium oxide fine powder from supply pipes 6 and 7. Afterwards, the glass disks were again washed with water.

Step 4) Laser beam irradiation of inner and outer peripheral edge surfaces.

Next, the glass disks for which the inner peripheral edge surface and the outer peripheral edge surface had been precision polished were taken one at a time, and the edge surfaces were smoothed by laser beam irradiation. The laser beam irradiation apparatus shown in FIG. 2 was used, and the smoothing processing conditions were as follows:

(1) Laser oscillator: Carbon dioxide laser (maximum rating 40W)

(2) Diameter of irradiated laser beam: Circle of diameter 3mm

(3) Laser power density: 4W/mm^2

(4) Laser beam irradiation method: Scan once across each part of edge surface (adjust to divergent beam using lens)

(5) Speed of rotation of glass disk at outer

The roughnesses of the inner and outer peripheral edge surfaces of the 500 samples of glass substrates for magnetic disks prepared using the method of Example 1 were recorded onto a chart using a stylus type roughness meter, and the average roughness Ra and the maximum roughness Rmax were calculated in accordance with a JIS-stipulated method. The results are shown in the "Example 1" row in Table 2.

The average roughness Ra of the samples prepared using the method of Example 1 was low at 0.03 to 0.06 μ m, and moreover the range over which the Ra value varies was also small. The average roughness Ra obtained thus did not exceed 0.1 μ m, which is the value required for the glass disk to be suitable for use as a magnetic disk for high-density recording using a magneto-resistive head (an MR head or a GMR head). Furthermore, the maximum roughness Rmax was 0.2 to 0.5 μ m, and hence the maximum value of Rmax did not exceed 1 μ m, which is the value required for use in high-density recording.

A glass substrate for a magnetic disk is manufactured through a plurality of processing steps, and usually washing with water, alkaline water, acidic water, washing water or the like is carried out after each step. However, even by washing it is not easy to completely remove foreign matter (glass waste that arises through grinding and polishing, residual abrasive grains, dust from the air, metal powder worn off from machinery, etc.) attached to the edge surfaces of the glass substrate, especially in recessed parts. When the glass substrate is used as an information recording medium in a hard disk drive and rotated at high speed, there is a high probability of such attached matter flying off the surface of the information recording medium due to centrifugal force and attaching to the information recording surface. This results in an increased risk of

magnetic head crashes.

To reduce this risk, in general the washing is carried out thoroughly, and also roughness consisting of projecting and recessed parts on the edge surfaces of the glass substrate is reduced so that washing will be easier and foreign matter will be less likely to become attached. As shown in Table 2, in the case of the samples prepared using the method of Example 1, the average roughness R_a is $0.06\mu\text{m}$ or less and the maximum roughness R_{max} is $0.5\mu\text{m}$ or less, showing that the edge surfaces have been processed well.

Example 2

500 samples of glass substrates for information recording media were prepared using the same method as in Example 1, but only the precision polishing of step 3C described above was not carried out. As shown in Table 2, the ranges of the average roughness R_a and the maximum roughness R_{max} for the samples prepared using the method of Example 2 were about the same as for the samples prepared using the method of Example 1.

Example 3

500 samples of glass substrates for information recording media were prepared using the same method as in Example 1, but only the second stage grinding of step 3B and the precision polishing of step 3C described above were not carried out. As shown in Table 2, the ranges of the average roughness R_a and the maximum roughness R_{max} for the samples prepared using the method of Example 3 were shifted to slightly higher values compared with these ranges for the samples prepared using the method of Example 1, but were still satisfactory.

Example 4

500 samples of glass substrates for information recording media were prepared using the same method as in Example 2, but only a crystallized glass (75mass% SiO_2 ,

3mass% Al_2O_3 , 4mass% K_2O , 12mass% Li_2O , 2mass% MgO , 3mass% P_2O_5 , 1mass% ZnO) was used instead of the amorphous aluminosilicate glass as used in Example 1. As shown in Table 2, the ranges of the average roughness R_a and the maximum roughness R_{max} for the samples prepared using the method of Example 4 were about the same as for the samples prepared using the method of Example 2.

Comparative Example 1

500 samples of glass substrates for information recording media were prepared using the same method as in Example 1, but only the precision polishing of step 3C and the laser beam irradiation of step 4 were not carried out. The range of the average roughness R_a of the samples prepared using the method of Comparative Example 1 was 0.6 to 1.3 μm , showing that the edge surfaces obtained had a roughness about 10 times greater than in Examples 1 to 4. Moreover, regarding the maximum roughness R_{max} , some samples were obtained with a low value of R_{max} of 2.5 μm , but there were also samples for which R_{max} was high at 5 μm . The presence of samples for which R_{max} is high means that there is a high possibility of there being glass substrates for information recording media within a production lot for which the possibility of attachment of foreign matter as described above is high, and hence a fear arises that it may not be possible to produce information recording media with high reliability.

Comparative Example 2

With an aim of making the average roughness R_a and the maximum roughness R_{max} lower than for the samples prepared using the method of Comparative Example 1, 500 samples of glass substrates for information recording media were prepared using the same method as in Comparative Example 1, but only the precision polishing of step 3C was added to the wet processing steps; this

precision polishing was carried out after the first stage grinding of step 3A and the second stage grinding of step 3B. As shown in Table 2, the average roughness Ra of the samples prepared using the method of Comparative Example 2 was lower than for Comparative Example 1. However, even though some samples were obtained with a low value of Ra of 0.05 μ m, there were some samples with a value of Ra of 0.4 μ m, and hence the value of the average roughness Ra varied over a broad range covering a factor of about 10 as compared with the samples prepared using the method of Example 1. Moreover, regarding the maximum roughness Rmax, there were some samples having a high value of 2.5 μ m.

From the above, it can be seen that in the case of the samples prepared using the methods of Examples 1 to 4, the values of the average roughness Ra and the maximum roughness Rmax are distributed over a narrow range, but in the case of the samples prepared using the methods of Comparative Examples 1 and 2, the values of the average roughness Ra and the maximum roughness Rmax are distributed over a broad range.

Moreover, it can be seen that even in the case of the samples prepared using the method of Example 3 in which the only wet processing step carried out is first stage grinding to adjust the inside and outside diameters to predetermined values, it is possible to obtain low values and narrow distributions of the average roughness Ra and the maximum roughness Rmax. It can thus be seen that it is possible to reduce the number of processing steps.

FIG. 8 is a graph showing the frequency distribution of the average roughness Ra over 500 samples prepared using the method of Example 2 and 500 samples prepared using the method of Comparative Example 2. The average roughness Ra has a narrow distribution in the case of the

samples prepared using the method of Example 2, but a distribution about 8 times as broad in the case of the samples prepared using the method of Comparative Example 2. If hard disk drives were manufactured using glass substrates for magnetic disks having a roughness distribution such as that of the samples prepared using the method of Comparative Example 2, then because the roughness is high, one would anticipate that the probability of the problems described earlier occurring would be increased.

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